Mehigan lech



Background

- Janney coupler has not been significantly modified since 1873
- Any modifications must be shared for compatibility between all cars in use
- Little motivation for product development by manufacturers

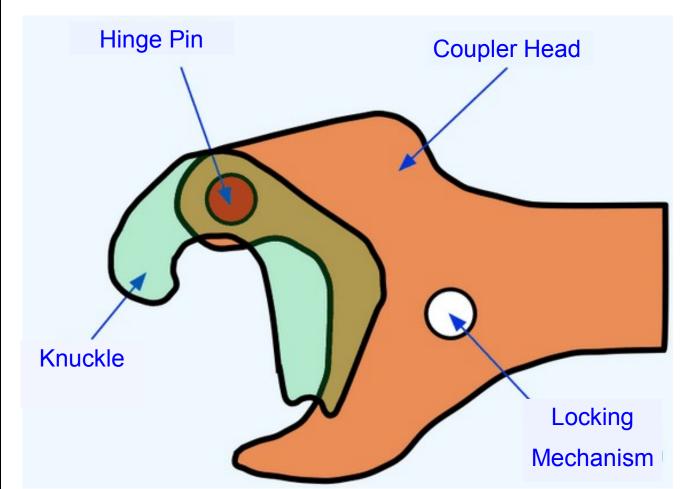


Photo credit:http://vnrailway.blogspot.com/2010/09/couplers.html

- Knuckle is fail safe to protect train car
- Want to fail in coupling face or around hinge pin
- Failure in tail section prohibits replacement in the field
- Knuckles fracture due to fatigue cracks



From left to right: Janney (1873), Type E (1930), Type F (1954)

- Couplers that fail in the field cause major delays
- Costs rail companies and customers time and money.
- Focus on knuckle which is most likely to fail



Type E made by Buckeye in 1976, provided by LS&I Railroad

No CAD model of the knuckle was

available, so the team created a

model by reverse engineering a

The knuckle was created in two

Design changes, due to FEA

results, circled in red.

type E coupler obtained from LS&I

Rail Car Coupler

Team 15: Francis Bremmer, ME Yidan Lou, ME Justin Tumberg, ME Kyle Pepin, CE Alyssa Sahr, MSE

Advisor: Dr. Paul van Susante



Design Considerations

Constraints

Constraint	Method of Measurement	Limits	
Backwards Compatible	Tested by Amsted Rail	Must fit 10-A contour gauge	
No change to car	Limit changes to knuckle	No change to freight car or coupler	
Standards	Meet AAR Regulations	Must meet minimum requirements	

Objectives

Objective	Priority Rating	Method of Measurement	Direction	Target Met
Life span	5	AAR Standard M-216	Maximize	In Progress
Strength	4	AAR Standard M-215	Maximize	In Progress
Weight	4	Weigh final product	Minimize	Yes
Cost	3	Cost of manufacturing	Minimize	No
Replacement Time	1	Down time caused by failure	Minimize	TBD

Prototype Realization

 Two part CAD Model translated into a mold pattern with Stereolithography (SLA) rapid

prototyping

Right: Example of knuckle mold pattern used by Amsted Rail



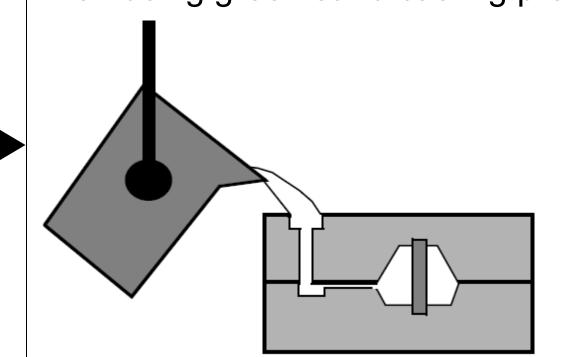


 Knuckles will have to fit standard AAR gauges, such as the A-10 contour gauge (shown left)

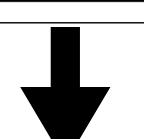


 Dynamic fatigue machine built by Amsted Rail will be used to evaluate the design

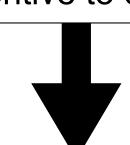




Left: Schematic of casting process from *Metal* Casting by Prof. Karl Rundman



 Knuckles will be commercially heat treated to undergo the process of austempering to form Austempered Ductile Iron (ADI). ADI was chosen because of similar properties to the current material, and excellent wear resistance. There is interest in the industry, but currently no incentive to develop further.



 Ship to Amsted Rail for performance testing on full scale static tensile and dynamic fatigue test equipment

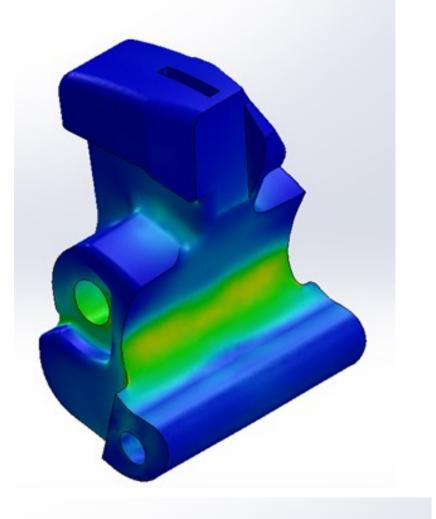




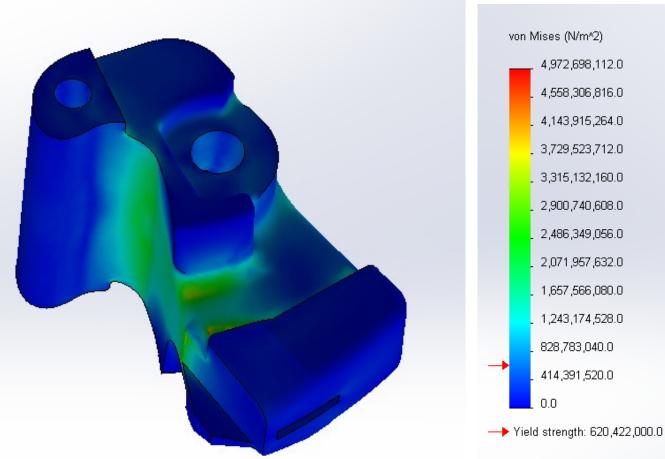
Client: Dr. Pasi Lautala External Industry Advisors: MaryClara Jones (TTCI), Darrell Krueger (BNSF), and Paul Wike (Amsted Rail)

Finite Element Analysis

To implement a material change, the static stresses in Austempered Ductile Iron (ADI) need to be less than or equal to Grade E steel. Due to the lower yield strength of ADI, trial and error was used to adapt material reductions within the knuckle, as shown in the CAD model. The simulations were run under two conditions, with and without the hinge pin as a fixture. By design, the pulling lugs should be the only fixture, as that is where the applied force on the face of the knuckle is transferred to. However, Amsted Rail found the hinge pin does act as a fixture when the knuckle is close to failure. The FEA shows what happens in normal use (no hinge pin) and when the knuckle is close to failure (hinge pin as a fixture).

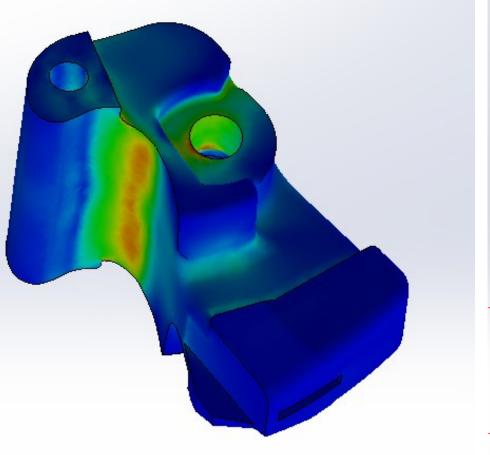


von Mises (N/m*2) Material: Grade E Steel 2,351,141,376.0 2,155,212,800.0 Fixtures: Hinge Pin and Pulling Lugs 1,959,284,480.0 **Load:** 650,000 lbf Result: Highest stresses occur near 1,175,570,688.0 hinge pin. Failures will occur in this 979,642,240.0 783,713,792.0 location. (Desired result) 587,785,344.0 391,856,896.0 195,928,448.0



Material: Grade E Steel Fixtures: Pulling Lugs Load: 650,000 lbf

Result: Highest stresses occur near hinge pin and pulling lugs. Failures will occur in either location. (Not ideal)



1,796,049,920.0 1,632,772,608.0 1,469,495,424.0 1,306,218,112.0 1,142,940,800.0 979,663,616.0 816,386,304.0 653,109,056.0 489,831,808.0 326,554,528.0 163,277,264.0

von Mises (N/m^2)

→ Yield strength: 620,422,000.0

von Mises (N/m^2)

___ 4,972,698,112.0

4,558,306,816.0

4,143,915,264.0

3,729,523,712.0

3,315,132,160.0

2,900,740,608.0

2,486,349,056.0

2,071,957,632.0

1,657,566,080.0

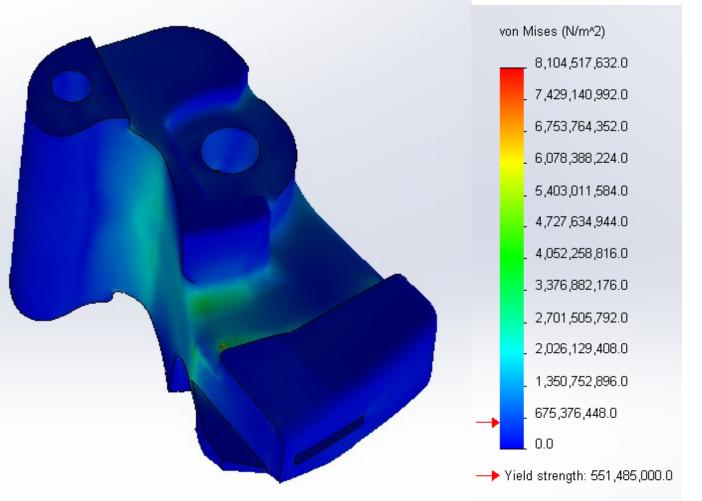
1,243,174,528.0

828,783,040.0

414,391,520.0

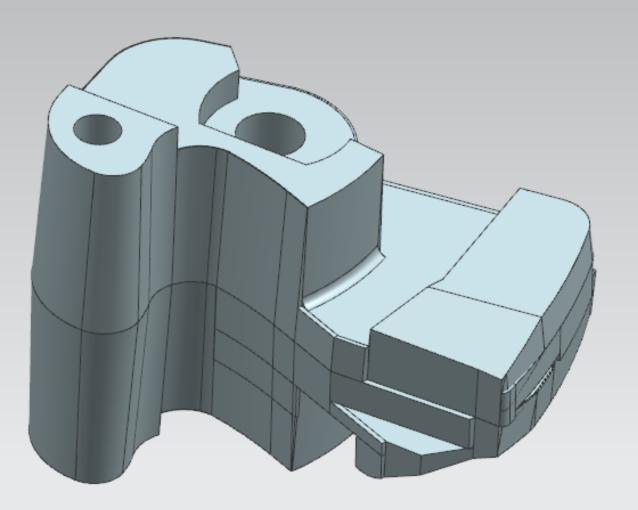
Material: ADI Fixtures: Hinge Pin and Pulling Lugs **Load:** 650,000 lbf

Result: Highest stresses occur near hinge pin. Failures will occur in this location. (Desired result)



Material: ADI Fixtures: Pulling Lugs **Load:** 650,000 lbf

Result: Highest stresses occur near hinge pin and pulling lugs. Failures will occur in either location. (Not ideal)



Assembled Knuckle

CAD Model

parts (shown below left and right) to enable modeling of inner cavities Draft angles were added to facilitate

Railroad

Bottom

